

# The Modal-Vertical-Beam(MVB) Transmission Loss Analysis

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## Report Documentation Page

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## Main Scientific Objective

- Extraction the beam-averaged modal attenuation coefficient  $d_n$

How to do?

Step 1: Perform vertical plane wave beamforming with VLA acoustic data

Step 2: Estimate the beamformer output spectrum

Step 3: Calculate propagation loss of two different ranges

Step 4: Extract the beam-averaged modal attenuation coefficient from propagation loss

Why to do?

Be important for bottom back-scattering matrix extraction from reverberation data as well as propagation modeling

# Theory Frame

The complex pressure in a range-independent waveguide can be written as:

$$p(r, z_j, z_s, w) = \sum_{n=0}^{N-1} a_n(r) \mathbf{j}_n(z_j) \mathbf{j}_n(z_s) \exp[-i(wt - k_n r + p/4) - d_n r]$$

For an ideal spatial filter response, the beamformer output can be written as:

$$b(r, \bar{\gamma}, z_s, \omega) = \sum_{m=-\Delta m/2}^{\Delta m/2} a_n(r) \varphi_n(z_s) \exp[-i(\omega t - k_n r + \pi/4) - \delta_n r]$$

The vertical beamformer output spectrum is

$$\begin{aligned} B(r, \gamma_n, z_s, \omega) &= \sum_n a_n^2(r) \varphi_n^2(z_s) \exp(-2\delta_n r) \\ &\quad + 2 \sum_n \sum_{m \neq n} a_n(r) a_m(r) \varphi_n(z_s) \varphi_m(z_s) \exp(-(\delta_n + \delta_m)r) \cos(\Delta k_{nm} r) \\ &= B_1 + B_2 \end{aligned}$$

## Theory Frame(continued)

If  $B_2 \ll B_1$ , the beamformer output spectrum is written as:

$$B(r, \gamma_n, z_s, \omega) = \sum_n a_n^2(r) \phi_n^2(z_s) \exp(-2\delta_n r)$$

We define the beam-averaged modal attenuation as follow:

$$\exp(-2\delta_{\bar{m}} r) = \frac{\sum_{\bar{m}-\Delta m/2}^{\bar{m}+\Delta m/2} a_n^2(r) \phi_n^2(z_s) \exp(-2\delta_n r)}{\sum_{\bar{m}-\Delta m/2}^{\bar{m}+\Delta m/2} a_n^2(r) \phi_n^2(z_s)}$$

Beam-averaged modal attenuation coefficient can be extracted by calculating the propagation loss for two ranges:

$$\delta_n = \frac{\log(tl(r_1, r_2))}{2(r_2 - r_1)} \quad \text{Where,} \quad tl(r_1, r_2) = \frac{B(r_1, \gamma_n, z_s, \omega) \times r_1}{B(r_2, \gamma_n, z_s, \omega) \times r_2}$$

# Numerical Simulation

We consider a Pekeris waveguide :  $H=103\text{m}$ ,  $C_0=1519\text{m/s}$ ,  $C_b=1623\text{m/s}$ ,  $\beta_b=1.72$ ,  $a_b=0.49 \text{ dB/m}\cdot\text{kHz}$ ,  $f=1390\text{Hz}$ . The 103m VLA is covered all depth of water column with 1m space of adjacent element.

Table 1 Theoretical value and calculated value of  $\delta_n$  in Pekeris waveguide ( $f=1390\text{Hz}$ )

group	Center grazing angle	Group of modes	Theory value of $\delta_n$	Calculated value of $\delta_n$	
				$r1=10\text{km}, r2=20\text{km}, z_s=20\text{m}$	$r1=10\text{km}, r2=20\text{km}, z_s=40\text{m}$
1	$2.3^\circ$	1-8	$3.367554\text{e-}6$	$-5.030152\text{e-}6$	$3.158571\text{e-}6$
2	$6.8^\circ$	9-16	$2.051041\text{e-}5$	$3.249568\text{e-}5$	$1.507090\text{e-}5$
3	$11.5^\circ$	17-24	$5.064872\text{e-}5$	$3.641855\text{e-}5$	$5.898481\text{e-}5$
4	$16.2^\circ$	25-32	$9.020034\text{e-}5$	$9.085626\text{e-}5$	$8.014695\text{e-}5$

Due to the effect of intermode interference ,  $\delta_n$  of group 1 can not be estimated correctly, and the precisions of estimated  $\delta_n$  of other groups are poor.

## Numerical Simulation(continued)

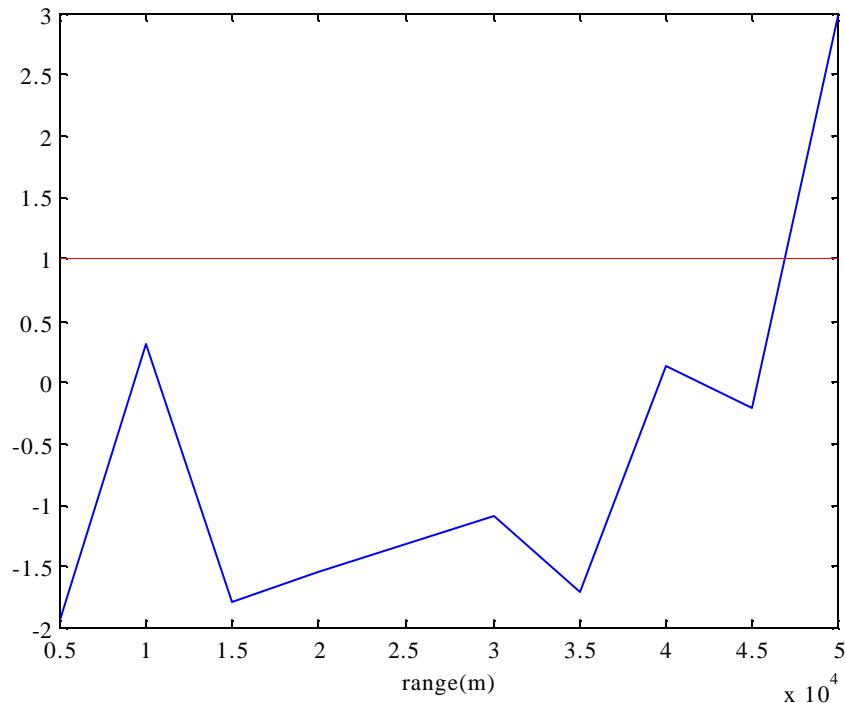
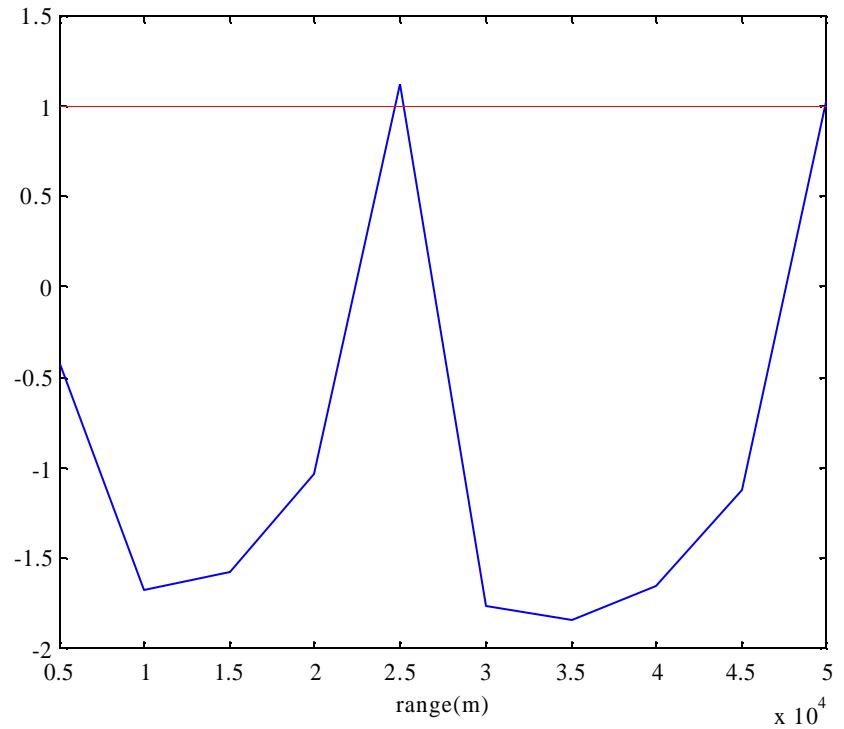


Fig.1 Effect of intermode interference  
( $f=1390\text{Hz}$ ,  $z_s=20\text{m}$ )

Fig.2 Effect of intermode interference  
( $f=1390\text{Hz}$ ,  $z_s=40\text{m}$ )

Effects of intermode interference  
can not be ignored



# Numerical Simulation(continued)

How can we reduce the effects of intermode interference? One method is averaged the beamformer output spectrum with  $f$  in a narrow band to smooth second item  $B_2$ .

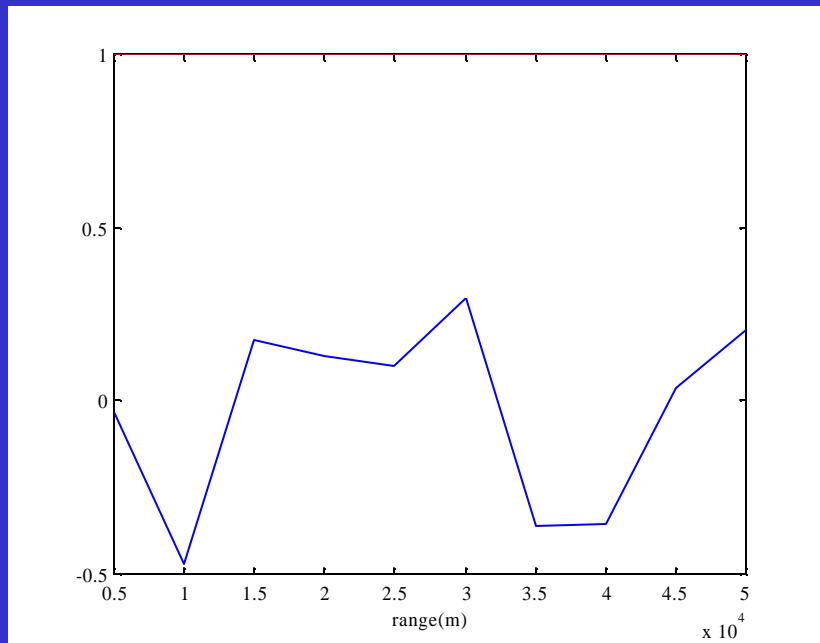


Fig.3 Effect of intermode interference ( $f=1340-1440\text{Hz}$ ,  $z_s=20\text{m}$ )

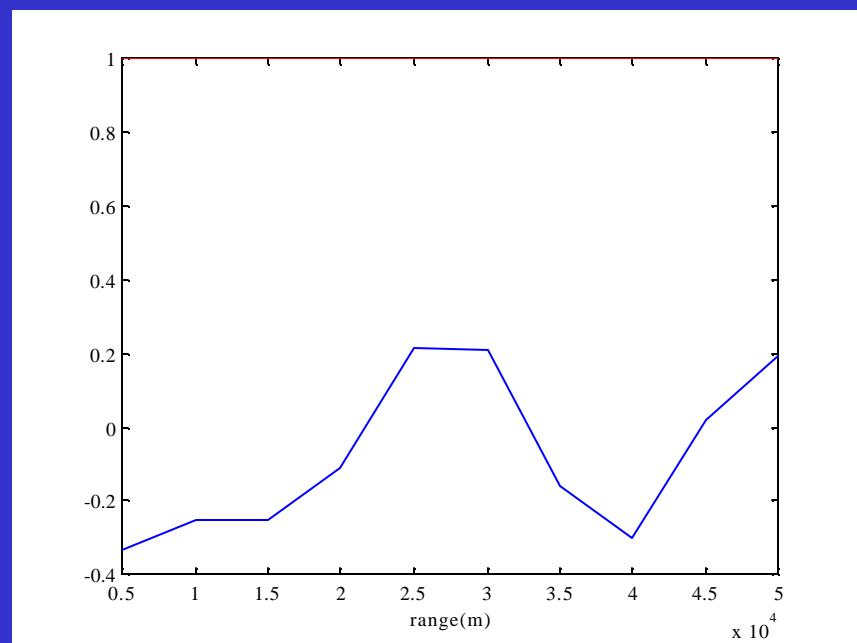


Fig.4 Effect of intermode interference ( $f=1340-1440\text{Hz}$ ,  $z_s=40\text{m}$ )



# Numerical Simulation(continued)

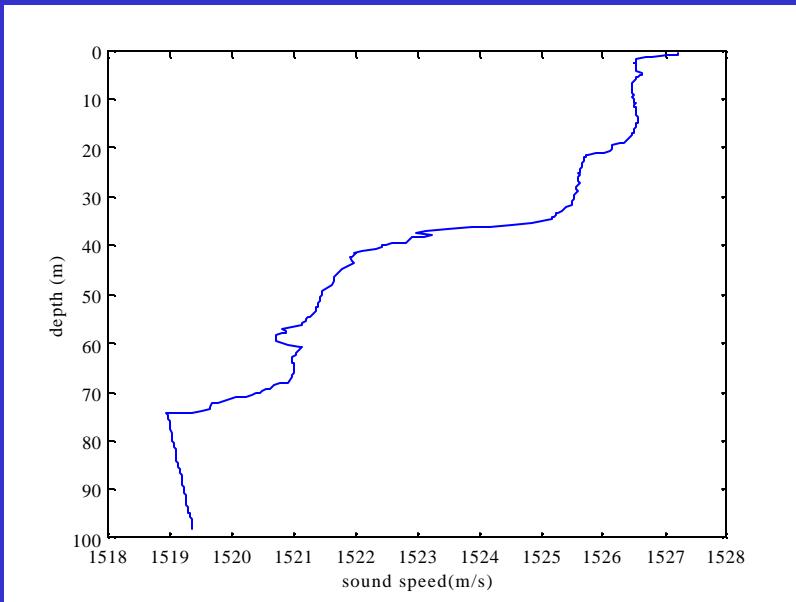
Table 2 Theory value and calculated value of  $\delta_n$  in Pekeris waveguide ( $f=1340-1440\text{Hz}$ )

group	Center grazing angle	Group of modes	Theory value of $\delta_n$	Calculated value of $\delta_n$		
				$r_1=5\text{km},$ $r_2=10\text{km},$ $z_s=40\text{m}$	$r_1=10\text{km},$ $r_2=20\text{km},$ $z_s=40\text{m}$	$r_1=10\text{km},$ $r_2=20\text{km},$ $z_s=20\text{m}$
1	2.3; $\tilde{a}$	1-8	3.143104e-6	7.894265e-6	1.705594e-6	3.646730e-6
2	6.8; $\tilde{a}$	9-16	1.918959e-5	1.920825e-5	2.095787e-5	1.802004e-5
3	11.5; $\tilde{a}$	17-24	4.754961e-5	4.799638e-5	4.731562e-5	4.815836e-5
4	16.2; $\tilde{a}$	25-32	8.491166e-5	8.500221e-5	8.566655e-5	8.432893e-5

Compared to Table 1, the attenuation coefficients of all groups can be estimated, the precision is also improved effectively.

# Numerical Simulation(continued)

Fig.  
5  
SVP  
of  
ECS



All the calculated  $d_n$  are larger than the theoretical values. This is due to:

- (1) effect of inter mode interference
- (2) the short VLA covered the upper half part of the water column is not able to capture the lower modes properly and affected by higher modes by leakage.

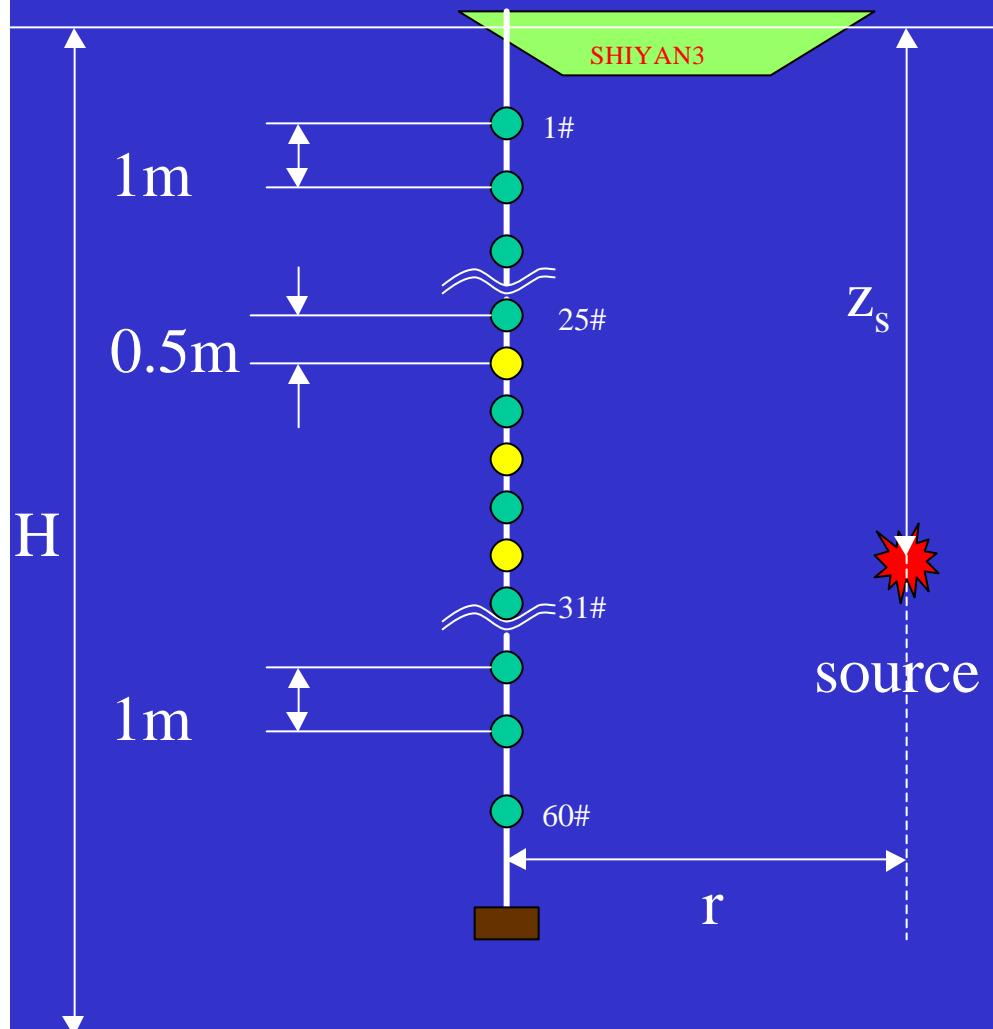
Table 3 Theoretical value and calculated value of  $\delta_n$  in simulated shallow waveguide ( $f=1340$ - $1440\text{Hz}$ )

group	Center grazing angle	Group of modes	Theory value of $\delta_n$	Calculated value of $\delta_n$	
				$r_1=10\text{km}, r_2=20\text{km}, z_s=40\text{m}, 103\text{mVLA}$	$r_1=10\text{km}, r_2=20\text{km}, z_s=40\text{m}, 57\text{mVLA}$
1	$2.3^\circ$	1-8	$6.011310\text{e-}6$	$2.193981\text{e-}5$	$1.630264\text{e-}5$
2	$6.8^\circ$	9-16	$2.272945\text{e-}5$	$3.075102\text{e-}5$	$4.356382\text{e-}5$
3	$11.5^\circ$	17-24	$3.601585\text{e-}5$	$5.283101\text{e-}5$	$6.074829\text{e-}5$
4	$16.2^\circ$	25-32	$8.115852\text{e-}5$	$8.317109\text{e-}5$	$1.071509\text{e-}4$

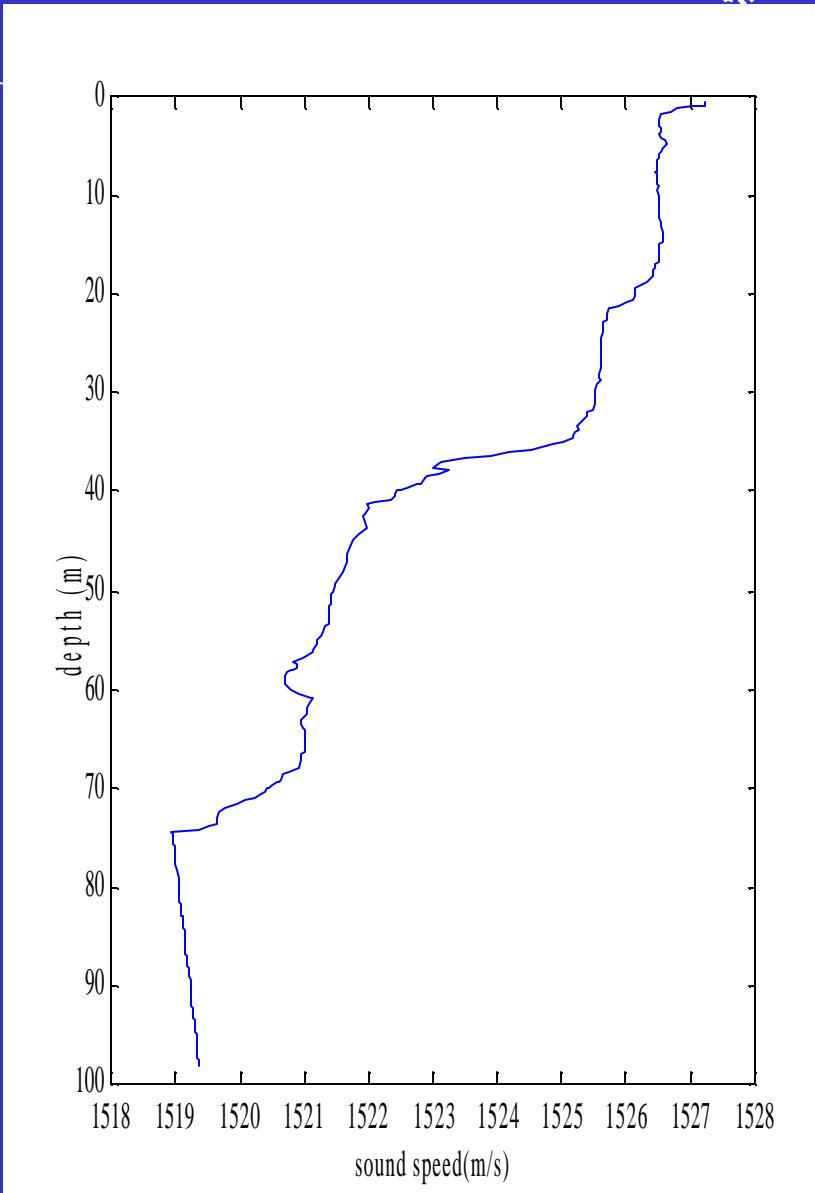
# ECS Real data analysis



## Experiment setup



● Not used in this paper



# ECS Real data analysis (continued)

## Experiment setup

- Receiving array: 60-element VLA, from 3m to 60m
- Source: locating at different depths  $z_s=5m, 20m, 40m$ , and different ranges  $r=5km, 10km, 20km$  and  $30\sim40km$
- Water depth:  $H=103m$
- Signal forms: 1100-2000Hz PRN, 630Hz CW, 630Hz PCW, 1250-2500HZ LFM, and explosive sources

In our talk, only signals of 1100-2000Hz PRN at ranges of 5km and 10km, depths of 20m and 40m are used to estimated beam-averaged  $\delta_n$  now.

# ECS Real data analysis (continued)

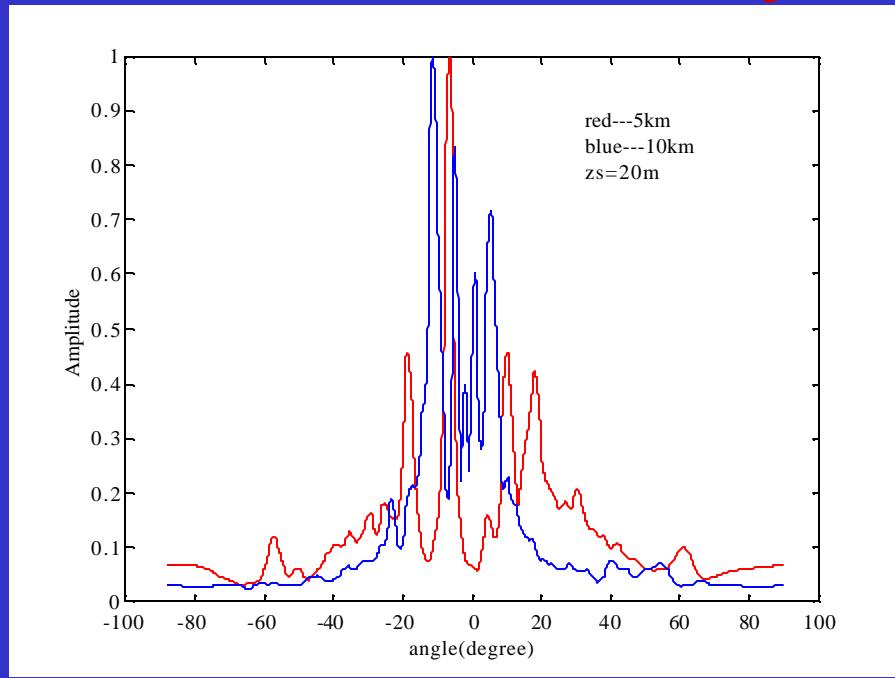


Fig.6 Vertical beam pattern with 20m source depth

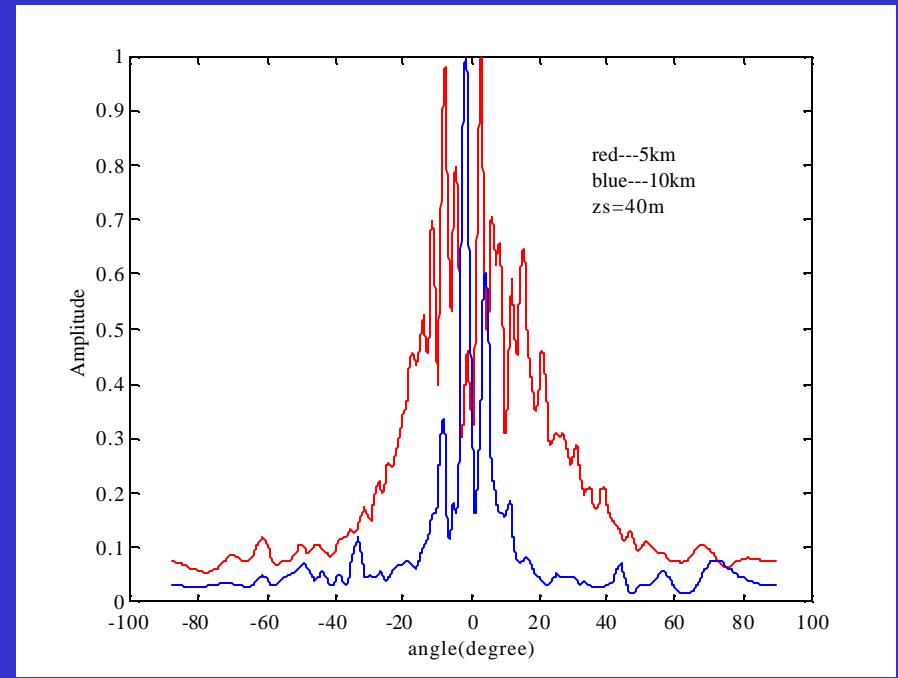


Fig.7 Vertical beam pattern with 40m source depth

Table 4 The estimated value of  $\delta_n$  in real shallow waveguide ( $f=1340$ - $1440\text{Hz}$ )

group	Center grazing angle	Group of modes	Estimated value of $\delta_n$	
			$r_1=5\text{km}, r_2=10\text{km}, z_s=20\text{m}$	$r_1=5\text{km}, r_2=10\text{km}, z_s=40\text{m}$
1	$2.3^\circ$	1-8	$1.195583\text{e-}4$	$2.785835\text{e-}5$
2	$6.8^\circ$	9-16	$2.447215\text{e-}4$	$1.224623\text{e-}4$
3	$11.5^\circ$	17-24	$1.853596\text{e-}4$	$1.175435\text{e-}4$
4	$16.2^\circ$	25-32	$2.953209\text{e-}4$	$1.934406\text{e-}4$

# Summary

- If the intermode sum can be ignored, the beamformer output spectrum of two different ranges can be used to extract beam-averaged modal attenuation coefficient.
- When vertical beamformer is performed in a narrow band not in single tone, the intermode sum can be reduced effectively, as proved by the numerical examples, but it is still large, should be decreased further.
- From numerical simulation and ECS real data analysis results, we should extract beam-averaged model attenuation coefficient from data collected by longer VLA covered all water column in a broader band.

Thank you!